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the cond. of glass electrodes are discussed. H. M.

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✓Electrical resistance, sodium error, asymmetric potential, hydrogen function, and chemical resistance of Sokolov-Pasynsky glass electrodes. František Čížek and František Stráfelda (Vysoká škola chem., Prag). Chem. Listy 49, 1954, 1105-1106, cf. Polj. C.I. 49, 1954, 1105. -- The electrical resistance of the electrode is expressed by the equation: $\log R_e = \log 0.01 - 0.008 (t - 25)$, where R_e is the resistance in MΩ at temperature t . The Na error from 50 to 90° in 0.01 molar Na⁺ solution was small; it is lower than for the Corning glass 015. A correction nomographic chart was constructed. The heating of the electrodes in H₂O at 150° for 80 hours has no effect on the asymmetric potential and on the value Δe in I/ΔpH. R. Frigg

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1. The potential of the 3.5 Nafion electrode
between 40° and 60° C. The potential of the
electrode was measured in a 0.1 M NaCl solution
at a constant rate of 10 mV/min. The potential
was measured between 40° and 60° C. The
measurements were made by means of a cell
consisting of a silver/silver chloride and a
hydrogen electrode in 0.1 M HCl. The
reference electrode was a 0.1 M HCl solution
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F

Abs Jour: Ref Zhur-Khin., No 24, 1958, 81415.

Author : Zavorcka J., Strafelda F.

Inst :

Title : Mercury Electrode With a Large Surface for the
Lengthy Polarographic Flow Measurements.

Orig Pub: Chem. listy, 1957, 51, No 12, 2374-2376.

Abstract: Described is the design of a polarographic cell, in which Hg, collecting from the dropper type electrode, is continuously diverted from the surface. In so doing, the surface is being continuously rejuvenated as Hg flows from the bottom of the cell into the dropper electrode. The described cell in conjunction with a recording instrument was in operation for 2 months in the service

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CZ/-60-5-8/35

Production of Machine Tools

500 mm; the machine is supplied by the TOS Kuřim, závod Lipník (TOS Kuřim Works, Lipník Plant). This lathe is equipped with a standardized hydraulic IKS type duplicating equipment, designed for turning diameters above the bearing of up to 900 mm. The author describes the principle of program control; Figure 2 shows the semiautomatic duplicating lathe SP 25 with program control, turning diameter above the bearing 250 mm, distance between centers 630 mm, motor output 22.5 kw, produced by the Kovosvit Plant in Sezimovo Ústí. It is equipped with two hydraulic duplicating supports and a support with several cutters for the machining of grooves. Figure 3 shows and explains the block-schematic of the program control equipment applied at the duplicating support of the SP 25 type lathe. Figure 4 shows the corresponding high-voltage control equipment and Figure 5 the low-voltage control equipment. Figure 6 shows the curveless one-spindle automatic lathe AB 80, designed for bar material of 80 mm, diameter of work pieces 240 mm when chucked, produced by the Kovosvit Plant at Sezimovo Ústí. It is equipped with an electro-hydraulic control and several supports. The vertical knee-type miller FB 40 v, shown on Figure 7, equipped with program control of the automatic operational cycle, has a chucking table of 400 x 1,800 mm, input 20 kw, produced by the TOS Plant at Kuřim. The description of automatic control and feed follows. Figure 10 shows and describes a block-schematic of the program control of an automatic miller by means of punched

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CZ/4-60-5-8/35

Production of Machine Tools

strips. The principle of control by punched strips is described in detail. Figure 8 shows the universal center grinder BJA 31 with program control device of the automatic cycle, type IMJ 28, turning diameter 315 mm, produced by the TOS Plant in Hostivař. The new designs of hob-type milling cutters for toothing are equipped with correcting devices decreasing deviations in machining of worm gearings to 0.003 mm per diameters of 1,000 mm. Figure 11 shows the IMOS type device measuring the circular thickness, produced by the TOS Plant in Čelákovice. A detailed description of this Czechoslovak invention, operating on the principle of magnetic gauging, follows. Figure 9 shows the horizontal boring machine WD 200, diameter of boring spindle 200 mm, produced by the V. I. Lenin Plants in Piseň. It is equipped with a centralized remote control; the boring spindle is placed in a four-sided spindle sleeve displaceable by 1,250 mm, the rotations of spindle are controllable in the range of 1 : 400. Figure 12 shows the automatic production line, machining journey boxes of railroad cars, produced by the TOS Plant in Kuřim. This line automatically performs 44 various operations; 9 operational stations form independent units, they are connected by conveying equipment for the feeding of boards with the chucked work pieces. The production line has a capacity of 14

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ACC NR: AP6027199

SOURCE CODE: CZ/6655/66/016/005/0409/0422

AUTHOR: Malek, Z.; Strahlova, J.; Fiala, J.; Novotny, J.

ORG: Institute of Radio Engineering and Electronics, Czechosl. Acad. Sci.,
Prague

TITLE: The influence of proper mechanical vibrations on some properties of TGS tandel (Paper read at the 2nd International Conference on Piezoelectricity in Liberec on Sept 1, 1965)

SOURCE: *Chekhoslovatskiy fizicheskiy zhurnal*, v. 16, no. 5, 1966, 409-422

TOPIC TAGS: mechanical vibration, tandel, flexural vibration, plane vibration, piezoeffect, permittivity, dielectric nonlinearity, frequency dependence

ABSTRACT: In the present paper the existence is proven of mechanical vibrations in TGS tandels in the frequency range from 5 kc/s to 1000 kc/s. A number of resonances were found in the given range of frequencies. Mainly plain and flexural vibrations occur. A study was made of their influence on the course of the

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ACC NR: AP6027199

frequency dependence of the complex effective permittivity, dielectric nonlinearities of the tandel, and the thermoelectric force measured by a thermocouple on its surface. From the study of the frequency dependence of these parameters at various temperatures the conclusion is drawn that the probable cause of the origin of mechanical vibrations in a tandel is the piezoeffect. The authors would like to express their gratitude to Ing. J. Janta of the Institute of Radio Engineering and Electronics, Czechoslovak Academy of Sciences, to Associate Professor Dr. J. Tichy of the Technical University in Liberec and to Dr. J. Mastner of the Institute of Radio Engineering and Electronics for valuable discussions and suggestions, and to Associate Professor Dr. O. Taraba of the Czech Technical University for facilitating the ultrasonic experiments and helping to arrange them in his laboratory. The authors are also indebted to all their colleagues for their friendly help. Orig. art. has: 7 figures and 2 formulas. [Authors' abstract] [KS]

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OTH REF: 009/

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406-411 K'63.

1. Ceske vysoke uceni technicke, Praha.

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Jan Straka. Inz stavby 12 no. 2: 88 P '64.

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Photographic properties of cyanine dyes I. Imidazo[1,2-a]pyridine carbocyanines. Chem prum 12 no.7:348-350 J1 '62.

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Z/017/62/051/003/001/002
D291/D304

AUTHORS: Straka, Jaronir, Engineer, and Kloss, Albert
TITLE: Degassing sealed ignitrons
PERIODICAL: Elektrotechnický obzor, v. 51, no. 3, 1962, 101 - 105

TEXT: This article generally describes the physical principles and design features of sealed rectifier ignitrons and lists the degassing and sealing method applied by the CKD Works in Prague. After initial degassing by electrical heating to 450°C and evacuation at 10-5mm Hg for 10 hrs., the CKD uses a simple and very accurate method to test the tightness of the tube: the ignitron is temporarily sealed, the grids are in contact with the pool, and a 24 kv a-c is applied to determine the anode-cathode stability. In case the tube is not sufficiently tight and degassed, the increased pressure impairs the electrical stability and a glow discharge can be observed between the electrodes. After this test, the seal is broken, and the tube is further degassed in the so-called 'forming' process. In this process, the igno-

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D291/D504

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tron is again evacuated and heated by applying a low voltage current which is gradually increased till 1.5 - times the nominal ignitron current is reached. The forming process is performed on a stand which permits the following test procedure: the ignitron is loaded with its nominal current and the exhaust pumps are disconnected. After a period of two hours, the current is also cut off, and the tube cooled for a period of four hours with the exhaust pumps still disconnected. The pressure is continuously measured through-out the entire test. During the period where the tube is loaded with its nominal current, the pressure rises only slightly; as soon as the arc is extinguished, the gettering effect of the current ceases, and the pressure rises considerably till reaching a certain maximum. This maximum is a criterion for the degassing degree and must not exceed a certain value. When this test is successfully passed, the ignitron is ready for final sealing. The sealing requires great care and is performed under continuous evacuation. The glass exhaust tube is degassed by repeated electrical red heating, and fused and cut with pneumatically operated jaws. After

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completion, the ignitron is again tested for its electrical stability by applying a tension of 24 kv between the anode and the grid which is connected to the cathode. There are 9 figures.

ASSOCIATION: CKD Praha (CKD Prague)

SUBMITTED: April 26, 1961

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Card 3/3

STRANA, Jaromir.

Primary malignant melanoma of the rectum. Rozhl. chir. 34 no.2:
129-133 F '60.

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dr. Jiri Novotny [diseased].
(MELANOMA case reports)
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Important information on the nailing of wooden containers.
Drevo 18 no.10:361-364 6 '63.

1. Vyzkumny a vyvojovy ustav drevarsky, Praha.

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Czechoslovak Standard: Impregnated wood ties. Drevo 18 no.9:
345-346 S '63.

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Z/026/60/C05/C01/C05/C05
B112/B202

16 0800

AUTHOR: Straka, Josef

TITLE: Contribution to the algebra of the isobaric spin

PERIODICAL: Aplikace Matematiky, v. 5, no. 1, 1960, 63-71

TEXT: According to V. Votruba and M. Lokajíček (Ref.1: An Algebraic System of Fundamental Particles. Publikace Spojeného ústavu jaderných výzkumů, Dubna 1958). the spin operators of particles with strong interaction (baryons, mesons) corresponding to the spin values $I = 0, 1/2, 1$ constitute an algebra which is characterized by the following relations:

$$(1) \quad \lambda_j \lambda_k - \lambda_k \lambda_j = i \epsilon_{jkl} \lambda_l$$

$$(2) \quad [\omega_j, \lambda_k] = i \epsilon_{jkl} \omega_l$$

$$(3) \quad \omega_j \omega_k \omega_l + \omega_l \omega_k \omega_j + \omega_k \omega_l \omega_j + \omega_j \omega_l \omega_k + \omega_l \omega_j \omega_k + \omega_k \omega_j \omega_l = 2(\delta_{jk} \omega_l + \delta_{kl} \omega_j + \delta_{lj} \omega_k)$$

$$(4) \quad \lambda_j \omega_k + \lambda_k \omega_j = \delta_{jk} U$$

$$(5) \quad U = 2/3 \lambda_j \omega_j$$

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